

Adhesion of single bacterial cells in the micronewton range

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The adhesion of bacteria to surfaces plays critical roles in the environment, disease, and industry. In aquatic environments, *Caulobacter crescentus* is one of the first colonizers of submerged surfaces. Using a micromanipulation technique, we measured the adhesion force of single *C. crescentus* cells attached to borosilicate substrates through their adhesive holdfast. The detachment forces measured for 14 cells ranged over 0.11 to 2.26 μN , averaging $0.59 \pm 0.62 \mu\text{N}$. Based on the calculation of stress distribution with the finite element analysis method (dividing an object into small grids and calculating relevant parameters for all of the elements), the adhesion strength between the holdfast and the substrate is $>68 \text{ N/mm}^2$ in the central region of contact. To our knowledge, this strength of adhesion is the strongest ever measured for biological adhesives.

adhesive strength | *Caulobacter crescentus* | cell mechanics | holdfast | micromanipulation

In the environment, bacteria are typically attached to surfaces as individual cells or as part of a biofilm. Bacterial biofilms are often the cause of biofouling, for example, when they form in implanted catheters, in water distribution systems, or on the hull of ships. The strong attachment of single bacterial cells to a surface provides the critical first step in the biofouling process. Understanding the nature, biosynthesis, and properties of the adhesives that mediate this attachment to surfaces is essential for a full understanding of the mechanisms of biofouling and biofilm formation.

The Gram-negative bacterium *Caulobacter crescentus* is ubiquitous in aquatic environments (1) and is among the first colonizers of submerged surfaces, initiating the process of biofouling (2). *C. crescentus* has a dimorphic life cycle with a motile swarmer cell stage, during which the initial attachment to surfaces occurs (3), followed by differentiation of the swarmer cell into a nonmotile cell that contains a polar extension called a stalk. The stalk is tipped by the holdfast, a polysaccharide adhesion that mediates the strong attachment of stalked cells to surfaces. *C. crescentus* cells attached to a surface are capable of resisting washing with strong jets of water, suggesting that the attachment of single cells is extremely strong (4).

A force of such a magnitude is far outside the range of applicability of laser tweezers, which provide maximum working forces on the order of $\approx 100 \text{ pN}$. In contrast, atomic force microscopy (AFM) can provide surface adhesion force measurements for cells attached to solid substrates. However, the measured force is typically for the adhesion of the AFM tip to a cell surface, and the coupling is not strong enough to detach the cell completely from its substrate (5, 6). The AFM tip has also been used to push laterally in an attempt to scrape off single cells. The resulting forces were of a few nN to 200 nN in magnitude (7). Flow chamber experiments (8) provided adhesion force measurements for a population of cells by counting the number of cells that remained attached after hydrodynamic shear stress was applied. Micropipette techniques have been previously used in the 5-pN to 20-nN range to investigate receptor–ligand bonding dynamics (9–11). When used in the form of biomembrane force

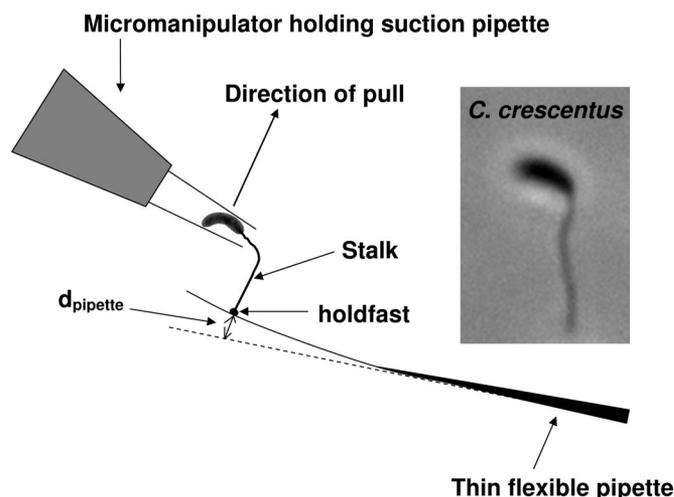


Fig. 1. Diagram of force measurement by micromanipulation. A single *C. crescentus* cell is attached to a thin flexible pipette. The bacterium is trapped in place at the tip of the suction pipette. The movement of the suction pipette is controlled by a micromanipulator, which pulls the bacterium up until the cell is detached. The suction pressure is applied by a syringe (not shown). (Inset) Image of a cell with an elongated stalk. (Magnification: $\times 3,000$.)

probes, micropipettes delivered forces ranging from 5 to 170 pN (12–15). These forces are still below what is needed for detachment of the single bacterial cells reported here.

In this article, we introduce a method for measuring the adhesion force of single bacterial cells with the ability to measure forces in the micronewton range. We find that the adhesion force of single *C. crescentus* cells reaches the order of micronewton, the largest ever measured for single bacterial cells to our knowledge.

Results

Force of Attachment of Single *C. crescentus* Cells. To measure the strong adhesion of *C. crescentus* to a solid substrate, we developed a micromanipulation method for measuring forces ranging from tens of nN to tens of μN (Fig. 1). Briefly, cells are allowed to attach to a thin flexible pipette whose force constant has been calibrated by AFM. A suction pipette is used to grab the body of an attached cell and pull the cell perpendicularly away from the flexible pipette. Because of the large force required, the cell body has to be sucked into the pipette, which is then bent away from the pulling direction. Thus the operation here differs from a recent study using the shear stress from continuous aspiration to detach much larger cells, the myotubes, from the substrate, which involves smaller forces generated by the fluid flow (16). In our setup, the force of adhesion is calculated from the amount

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Abbreviation: AFM, atomic force microscopy.

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stalk, at the stalk–holdfast junction, within the holdfast, and at the holdfast–surface interface. To determine the position of breakage, we grew *C. crescentus* on glass coverslips and then compared fluorescent holdfast images before and after vigorous rinsing with water. Coverslips where the cell bodies were washed away had the same density of holdfast labeling as undisturbed coverslips (data not shown). This finding suggests that the point of breakage is most likely above the holdfast–substrate junction. AFM images of the coverslips described above after rinsing showed numerous holdfasts, mostly without stalks but some with short stalk fragments. The images of the holdfasts from which the stalks were completely removed were similar to those left on a glass surface by holdfast attachment mutants that are unable to keep the tip of the stalk attached to the holdfast (17) (data not shown). These holdfasts did not have the appearance of craters, suggesting that the holdfast material to which the stalk tip was attached remained with the holdfast on the surface. We conclude that the breaking position was typically either at the holdfast–stalk junction or somewhere along the stalk.

AFM Measurement of the Size of Stalks and Holdfasts. We performed AFM imaging for 12 stalks to obtain an average diameter of $\approx 119 \pm 10$ nm after subtracting the AFM tip broadening effect of ≈ 60 nm for dried stalks with an average detected height ≈ 40 nm (based on the geometry for the tip known from the manufacturer). Using a stalk diameter of 119 nm and an average detachment force of $0.59 \mu\text{N}$, we found that the average threshold stress the stalk could endure was estimated to be 53 N/mm^2 , assuming the stalk to be a solid rod. If the stalk is considered a hollow wall, the stress that can be endured by the wall material ought to be larger, and inversely proportional to the cross-sectional area.

To determine the strength of the adhesion between the holdfast and the substrate, we needed to determine the area over which the force was transmitted. The size of 18 holdfasts was measured with AFM imaging as illustrated in Fig. 3; the diameter varied from 254 to 579 nm with an average of 411 nm (after subtracting the AFM tip size broadening of ≈ 26 nm on holdfasts with heights of ≈ 10 nm). The size of the holdfast has previously been shown to vary from cell to cell (17).

Finite Element Analysis of the Adhesion Strength of the Holdfast.

Because the holdfast spreads over a much larger area than the tip of the stalk, the stress within the holdfast and at the interfaces is no longer given by the simple formula of force/area. Instead, the stress and strain have to be calculated as tensors (each having up to 3×3 components) based on the known geometry and by assuming certain material properties of the holdfast. The deformation of the holdfast was simulated by means of the numerical finite element method. The material was assumed to be elastic based on our previous results (17), with a Young's modulus of 100 MPa (10^8 N/m^2) and a Poisson ratio of 0.4. This value of Young's modulus was chosen to be comparable to a strong matrix of biological origin such as the byssal thread of marine mussels (18). At the average detachment stress, the calculated strain is 0.53. A much lower value of Young's modulus, which might be more suitable for the holdfast material, would lead to a highly nonlinear strain field, which is impossible to calculate without knowing the form of the stress–strain relationship. In our calculation, a linear relationship between stress and strain is assumed to estimate the stress distribution. The Poisson ratio of 0.4 is commonly used for a wide range of materials with low compressibility, including glass and silk. The holdfast was modeled as a disk of diameter 411 nm and thickness 40 nm. This thickness was chosen on the basis of our previous measurements of wet holdfasts, showing that the holdfast thickness shrinks ≈ 3 -fold upon drying (17). The stalk was attached over a circular patch on the top surface of initial radius 59.5 nm (Fig. 3D),

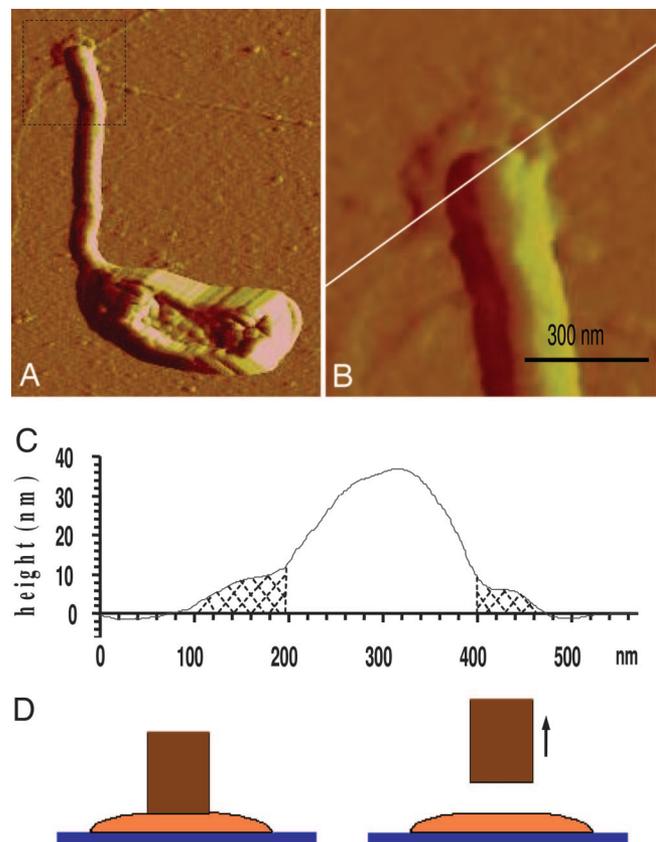


Fig. 3. Measurement of holdfast size and thickness by AFM. (A) AFM image of a *C. crescentus* stalked cell, grown on glass coverslip, with the holdfast at the end of the stalk. (Total scan area: $3 \mu\text{m} \times 2.4 \mu\text{m}$.) (B) Enlarged image of the holdfast area. The height is measured along the white cross cut. (C) Plot of the height of the dried holdfast. Shaded regions in the plot indicate the visible holdfast area. For 18 sampled cells, the area of the holdfast ranged from 254 to 579 nm in diameter, and the average value obtained was 411 nm. (D) Schematics showing that when a cell is pulled off the glass substrate the stalk (brown) detaches from the holdfast (orange).

imposing uniform displacement in the normal or z -direction where the force is applied. The bottom of the disk was constrained against displacement in the z -direction.

Fig. 4 shows the deformation at a total force of $0.59 \mu\text{N}$ for the central portion of the disk of radius 59.5 nm. The contour plot in Fig. 4A shows level curves of the tensile stress component σ_{zz} throughout the axially symmetric configuration. The graph in Fig. 4B shows in detail the distribution of this stress component at the interface of the holdfast with the stalk (solid curve) and substrate (dashed curve). The solid curve in Fig. 4B, labeled top surface, shows the normal stress exerted in the disk by the stalk over the planar contact surface. The stress is much larger at the interface between the holdfast and the stalk, especially at the edge, which is likely the reason it is easier for detachment to occur at this interface rather than between the holdfast and substrate. The dashed curve in Fig. 4B shows the normal stress exerted by the rigid glass substrate on the base of the disk. The maximum stress at the holdfast–substrate interface is 68 N/mm^2 in the central region. The interface is not broken under this force, indicating that the strength of adhesion of the holdfast to the substrate is larger than this value. The integrated force of either distribution is equal to the pulling force.

The integrity of the holdfast GlcNac polymers is critical for the strong adhesion of *C. crescentus* cells. The only characterized component of the holdfast is polymers of GlcNac (19). We have

experiments, but were allowed to attach to glass coverslips. After rinsing, the coverslips were dried and imaged in air by using contact mode.

Measurement of Detachment Force by Micromanipulation. To detach a *C. crescentus* cell from the flexible micropipette, a suction micropipette was approached to the attached cell. The suction pipette was mounted on a NanoControl micromanipulator (Kleindiek Nanotechnik, Reutlingen, Germany). This micromanipulator can move in incremental steps of 50 nm to 1 μm . Suction pressure was produced by a Stoelting 51222 Manual Microsyringe Driver with a Hamilton 710LT 100- μl syringe. Once a cell was held in place just inside the tip of the suction pipette, we began videotaping while pulling the cell perpendicularly away from the thin flexible pipette to which the cell was attached. The position at which the cell detachment event was observed yielded the cell's adhesion force.

Deflection measurements were made by using a Nikon TE-2000U inverted microscope with a $\times 100$ objective designed for phase contrast and fluorescence imaging. Cells were labeled with NanoOrange. Pulling movies were recorded by using a Marshall V-1070 black and white charge-coupled device camera and a Sony GV-D800 digital video recorder. Cells attached to the pipette through their holdfast with their body aligned in the direction of the suction pipette were used. Let the deflection of the flexible micropipette to which a cell was attached be d_{pipette} , and the force constant or elastic stiffness of the pipette be k_{pipette} . The pulling force, F , which was counterbalanced by the bending pipette, was obtained by Hooke's law, $F = k_{\text{pipette}} \cdot d_{\text{pipette}}$.

Measuring the Force Constant of the Flexible Micropipette. To calibrate the force constant at the position of cell detachment, we used AFM (Dimension 3100, Digital Instruments) in contact mode and tipless calibration cantilevers with force constant, $k_{\text{cantilever}}$, of 0.71 N/m. At equilibrium, the force of the thin flexible glass pipette balanced the elastic force of the cantilever,

$$F_{\text{pipette}} = k_{\text{pipette}} \cdot d_{\text{pipette}} = k_{\text{cantilever}} \cdot d_{\text{cantilever}}$$

The elastic deflections of the pipette, d_{pipette} , and cantilever, $d_{\text{cantilever}}$, were generated by the AFM's piezo electric tube such that for small angles,

$$d_{\text{tube}} = d_{\text{cantilever}} + d_{\text{pipette}}$$

Knowing the deviation of the AFM tube, d_{tube} , and deviation of the cantilever, $d_{\text{cantilever}}$, we obtained the deviation of our pipette, d_{pipette} . With a known force constant of the cantilever, $k_{\text{cantilever}}$, we obtained the force constant of the pipette, k_{pipette} . Hence,

$$k_{\text{pipette}} = k_{\text{cantilever}} \cdot d_{\text{cantilever}} / (d_{\text{tube}} - d_{\text{cantilever}}).$$

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