

Miniature curved artificial compound eyes

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In most animal species, vision is mediated by compound eyes, which offer lower resolution than vertebrate single-lens eyes, but significantly larger fields of view with negligible distortion and spherical aberration, as well as high temporal resolution in a tiny package. Compound eyes are ideally suited for fast panoramic motion perception. Engineering a miniature artificial compound eye is challenging because it requires accurate alignment of photoreceptive and optical components on a curved surface. Here, we describe a unique design method for biomimetic compound eyes featuring a panoramic, undistorted field of view in a very thin package. The design consists of three planar layers of separately produced arrays, namely, a microlens array, a neuromorphic photodetector array, and a flexible printed circuit board that are stacked, cut, and curved to produce a mechanically flexible imager. Following this method, we have prototyped and characterized an artificial compound eye bearing a hemispherical field of view with embedded and programmable low-power signal processing, high temporal resolution, and local adaptation to illumination. The prototyped artificial compound eye possesses several characteristics similar to the eye of the fruit fly *Drosophila* and other arthropod species. This design method opens up additional vistas for a broad range of applications in which wide field motion detection is at a premium, such as collision-free navigation of terrestrial and aerospace vehicles, and for the experimental testing of insect vision theories.

bioinspired robotics | wide-angle vision | optic flow sensor | Micro-opto-electromechanical systems

Insect compound eyes consist of a mosaic of tiny optical units, or ommatidia (1). Compared with vertebrate single-lens eyes, compound eyes offer a versatile morphology with panoramic field of view (FOV), negligible distortion and aberration, and high temporal resolution, while trading high spatial resolution for diminutive size (2). These features are particularly beneficial for visually controlled navigation, including tasks like collision avoidance, take-off, landing, and other optomotor responses that do not require a high density of photoreceptors. Insect compound eyes possess local sensory adaptation mechanisms capable of compensating for large changes in light intensity right at the photoreceptor level (3, 4), and they wrap around highly distributed neuronal circuitry, allowing for fast and low-power integrated signal processing (5), whereas minimizing the overall size of the insect head. An artificial compound eye exhibiting all these properties would represent an ideal miniature sensor for numerous situations in which fast motion detection across wide FOVs is required (6–9).

Attempts have recently been made to develop miniature compound eyes. Both planar (10) and curved (11–14) microlens arrays have been fabricated. In some cases, these were interfaced with conventional flat CMOS arrays, but this resulted in off-axis aberrations, crosstalk between neighboring ommatidia, or limited FOV. At first sight, recent developments in flexible sensors (15–18) could represent a promising avenue for curved vision sensors (19, 20). However, adapting those flexible technologies to the design of curved compound eyes is challenging due to the recurring problem

of precisely aligning a curved photodetector array with a curved microlens array. None of these previous methods or other available omnidirectional camera systems (21) display important features of biological compound eyes, such as embedded data processing, versatile morphologies, high temporal resolution, and local light adaptation in a miniature package.

Here, we describe a unique approach to the design of a curved artificial compound eye, named CurvACE. We validate this approach by characterizing the sensitivity, angular resolution, and motion extraction capabilities of a prototype bearing a semicylindrical morphology (Fig. 1A) and a hemispherical FOV of $180^\circ \times 60^\circ$ (Fig. 1B). This prototype is a self-contained, integrated, curved artificial compound eye system with morphology and properties resembling those of primitive (22) (Fig. 1C) and modern (1) (Fig. 1D) arthropods. In particular, the CurvACE prototype features several similarities with the eye of the fruit fly *Drosophila*, namely, spatial resolution, acceptance angle, number of ommatidia, local light adaptation, crosstalk prevention, and signal acquisition bandwidth, as well as a smaller but comparable FOV (Table 1). Such curved visual sensors may be useful for terrestrial and aerial vehicles, medical instruments, prosthetic devices, home automation, surveillance, motion capture systems, and smart clothing. Artificial compound eyes may also foster the development of alternative visual algorithms, and when fitted on physical robots, they could help explore fundamental principles in animal sensory-motor control (6, 8, 9, 23).

Fabrication Process

Design Method. As with biological compound eyes, CurvACE artificial ommatidia consist of three materially and functionally different layers (Fig. 2A): (i) an optical layer composed of an array of highly transparent polymer microlenses molded on a glass carrier (Fig. S1), which focus light precisely onto (ii) the sensitive areas of a silicon-based photodetector layer. This layer contains an array of analog very-large-scale integration (VLSI) photodetectors as well as additional circuitry to condition the signal for processing (Fig. S2). Finally, (iii) a flexible electromechanical interconnection layer, formed by a polyimide printed circuit board (PCB), physically supports the ensemble and transfers the output signals from the individual ommatidia (Fig. 2B) to the processing units. With thicknesses of 550 μm , 300 μm , and 100 μm , respectively, the total

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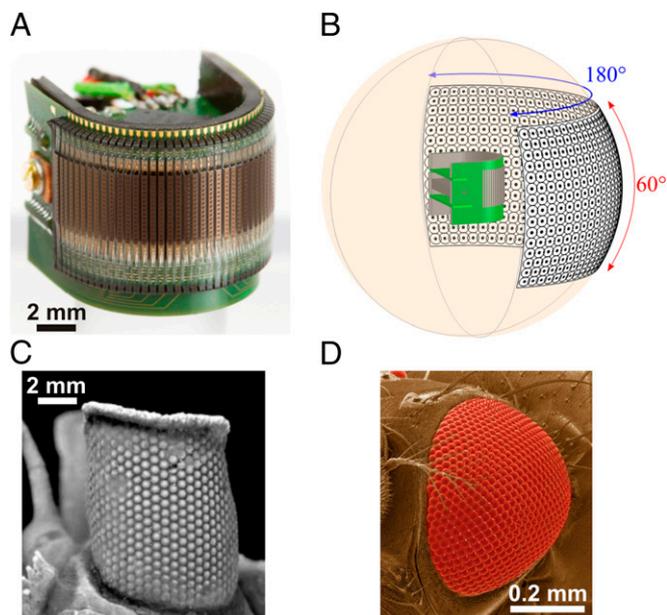


Fig. 1. Artificial and natural curved compound eyes. (A) Image of the CurvACE prototype. The entire device occupies a volume of 2.2 cm³, weighs 1.75 g, and consumes 0.9 W at maximum power. (B) Illustration of the panoramic FOV of the fabricated prototype. The dots and circles represent the angular orientation and acceptance angle $\Delta\rho$ of every ommatidium, respectively. Compound eye of the extinct trilobite *Erbenochile erbeni* (22) (C) and of the fruit fly *Drosophila melanogaster* (D). [(C) Reprinted from ref. 22 with permission from AAAS; (D) Reprinted from ref. 44 with permission from AAAS.]

height of the three assembled layers is less than 1 mm in the prototype presented here.

The apposition and neural superposition compound eyes of many arthropod species contain pigmented sidewalls that contribute to reducing optical crosstalk between ommatidia (1). Our solution to suppress optical crosstalk makes use of two low-reflective opaque metal layers with matching pinhole patterns: one subjacent to the microlens array and the other one close to the focal plane, ahead of the photodetector layer (10) (Fig. 2A and B and Fig. S1C).

The proposed design method is based on a planar fabrication technology for each of the three layers of the artificial ommatidia array, followed by high-precision cutting (dicing) of the rigid ommatidia layers to add bendability. Specifically, each of the three layers is fabricated at first with wafer-level (optical and photodetector layer) or batch-level (interconnection layer) processes using

standard microengineering technologies (Figs. S1 and S2). Next, the optical and photodetector layers are aligned at micrometer accuracy and glued chip-wise (Fig. 2B). Subsequently, the ensemble is fixed and wire-bonded to the electromechanical interconnection layer. Finally, the rigid optical and photodetector layer stack is precisely separated with a chip dicing saw in columns of ommatidia down to the flexible interconnection layer, which remains intact (Fig. 2C and Fig. S3A). This procedure ensures accurate and reproducible alignment of the optical and photosensitive elements across the array while providing electronic accessibility to the output signals of the individual artificial ommatidia. It results in a very thin and light package, less than 1 mm and 0.36 g in the prototype presented here, and ensures mechanically safe bending of the interconnection layer down to a small radius of curvature (Fig. 2D). Free space on the backside of the artificial ommatidia permits attachment to curved rigid or flexible substrates and incorporation of additional electronics for signal processing in the resulting concavity (Fig. 2D).

Fabrication of a CurvACE Prototype. We fabricated a CurvACE prototype by bending a rectangular array of 42 columns of 15 artificial ommatidia (microlens diameter = 172 μm) down to a curvature radius of 6.4 mm along its longer direction to yield a 180° FOV in the horizontal plane (Fig. 1A and B and Fig. S3B and C). This curvature should nominally yield an interommatidial angle $\Delta\phi_h$ of 4.3° in the equatorial row along the bent direction. Although there is no mechanical bending along the vertical direction, it is possible to make the visual axes of the 15 ommatidia in each column fan out in the vertical plane by making the vertical pitch between the photodetectors stepwise smaller than the vertical pitch between the microlenses (10) (Fig. S1C). In the prototype, the photodetector pitch was calculated so as to obtain a similar value for the interommatidial angle $\Delta\phi_v$ along the vertical unbent direction, which results in a total vertical FOV of 60° (Fig. 1B). To avoid spatial aliasing or blind spots in the visual field, the acceptance angle $\Delta\rho$ of each ommatidium must closely approach the interommatidial angle $\Delta\phi$ (1, 24) (Fig. 3C). Therefore, the ommatidial lenslets, diaphragms, and photodetectors were designed using an optical ray tracing technique (Zemax; Radiant Zemax, LLC) to produce an acceptance angle $\Delta\rho$ of 4.3°.

The resulting concavity on the backside of the prototype after the mechanical bending along the horizontal direction is used to host two microcontrollers, two inertial sensors, and other electronic components that are fitted and soldered on two rigid PCBs (Fig. 2D and Figs. S3C and S4). In the experiments described below, the embedded microcontrollers are programmed to operate the visual data read-out and communicate with an external computer for analysis; in a stand-alone application, these microcontrollers can be used to process visual data onboard the prototype without any external computer.

Results

Characterization of Visual Sampling. To characterize the visual sampling of the environment by the fabricated CurvACE prototype, we measured the angular sensitivity function (ASF) of each of the 630 artificial ommatidia (Fig. S5). Fig. 3A and D shows representative examples of ASFs measured along a single row and a single column, respectively. Most ASFs display the expected Gaussian distribution with respect to the light incidence angle, which validates both the microoptical design and the precise alignment with each individual photodetector. We derived the experimental acceptance angles and interommatidial angles from the measured ASFs. The acceptance angle $\Delta\rho$ of an ommatidium is defined as the full width at half maximum (FWHM) of its Gaussian-like ASF. The horizontal and vertical interommatidial angles $\Delta\phi_h$ and $\Delta\phi_v$ were assessed from the angular position of the peak of the ASFs of two adjacent ommatidia (Fig. 3C). The measured acceptance angles yielded an average of $\Delta\rho$ of $4.2^\circ \pm 0.3^\circ$ (SD) for both

Table 1. Specifications of CurvACE prototype compared with the characteristics of the *Drosophila melanogaster* compound eye

	CurvACE	<i>Drosophila</i> eye [Ref(s).]
Number of ommatidia	630	600–700
Facet diameter, μm	172	16 (42)
Eye diameter, mm	12.8	0.36 (42)
Facet diameter/eye diameter, %	1.3	4.4
Interommatidial angle, $\Delta\phi$; deg.	~4.2	~4.7–5.5 (42)
Acceptance angle, $\Delta\rho$; deg.	4.2	~4.5 (24)
FOV, deg.	180 × 60	160 × 180 (43)
Signal acquisition bandwidth, Hz	300	<100 (28)
Adaptability to illumination	Yes	Yes (4)
Crosstalk prevention	Yes	Yes (24)

deg., degree.

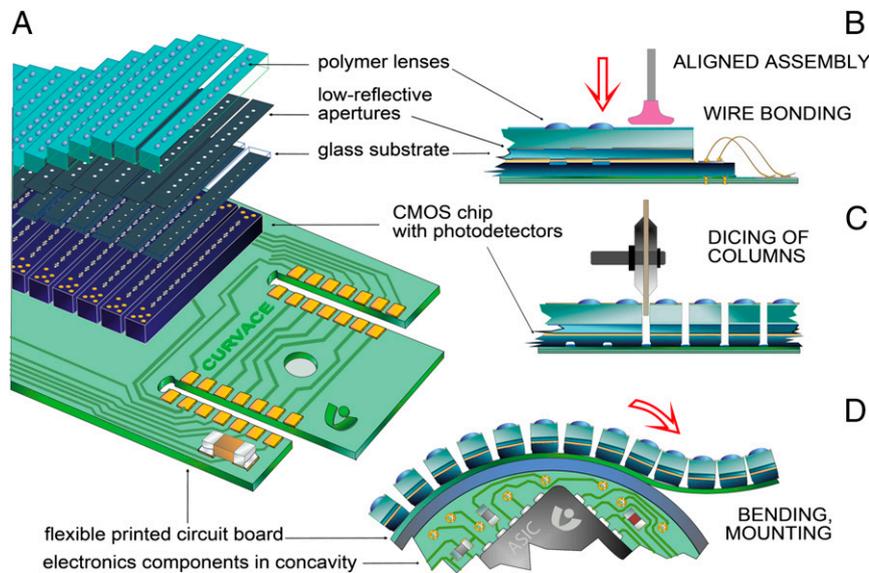


Fig. 2. CurvACE design and assembly. (A) Scheme of the three layers that compose the CurvACE artificial ommatidia: optical (microlenses and apertures), photodetector (CMOS chip), and interconnection (PCB). (B) Accurate alignment and assembly process of the artificial ommatidia layers in planar configuration. (C) Dicing of the assembled array in columns down to the flexible interconnection layer, which remains intact. (D) Curving of the ommatidial array along the bendable direction and attachment to a rigid semicylindrical substrate with a radius of curvature of 6.4 mm to build the CurvACE prototype. Two rigid circuit boards containing two microcontrollers, one three-axis accelerometer, and one three-axis rate gyroscope are inserted into the rigid substrate concavity and soldered to the sides of the ommatidia through dedicated pads (Figs. S3D and S4).

horizontal (Fig. 3A) and vertical (Fig. 3D) directions. The vertical interommatidial angles resulted in an average of $\Delta\phi_v$ of $4.26^\circ \pm 0.16^\circ$ (SD) (Fig. 3D), and the horizontal ones ranged from $\Delta\phi_h = 4.2^\circ \pm 0.8^\circ$ (SD) in the middle row (Fig. 3A) to $3.7^\circ \pm 0.7^\circ$ (SD) in

the top and bottom rows (Fig. 3B). The close match between the experimentally measured acceptance angles and interommatidial angles validates both the ray-tracing design and fabrication process while indicating that the CurvACE prototype, like the

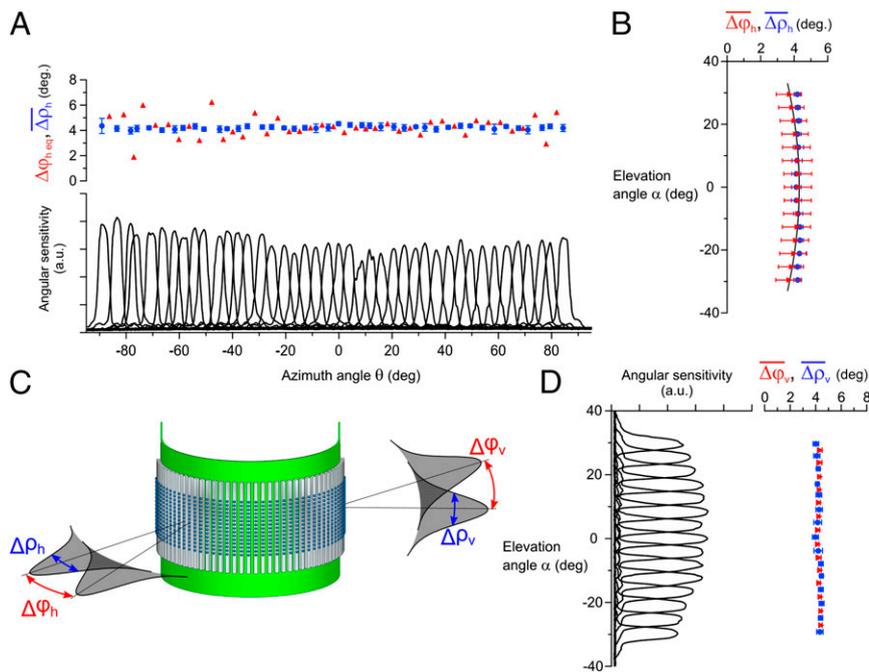


Fig. 3. Characterization of CurvACE angular sensitivity. (A) Measured ASF along the middle (equatorial) row (black curves), with the corresponding interommatidial angles $\Delta\phi_{h,eq}$ (red triangles) and mean acceptance angles $\Delta\rho_h$ (blue circles) of the CurvACE ommatidia averaged along every column. Error bars display SDs. (B) Mean horizontal interommatidial and acceptance angles averaged along every row of artificial ommatidia as a function of the elevation angle α . The black curve shows the theoretical $\Delta\phi_h$ values obtained using Eq. S10 with a constant $\Delta\phi_{h,max}$ of 4.2° . (C) Schematic representation of the acceptance angle $\Delta\rho$ of an ommatidium and the interommatidial angle $\Delta\phi$ calculated from the peak ASFs of two neighboring ommatidia. (D) Measured ASFs along a single column of artificial ommatidia (black curves), mean vertical interommatidial (red triangles), and acceptance angles (blue circles) averaged along every row of artificial ommatidia. a.u., arbitrary units; deg., degree.

fruit fly compound eye (24), performs an adequate sampling of its entire FOV (Fig. 1B). The observed spread in the values of the horizontal interommatidial angles $\Delta\phi_h$ (Fig. 3A and B) is probably due to the manual process used to mechanically fix the flexible PCB supporting the artificial ommatidia array onto the rigid curved substrate.

Characterization of Ommatidium Light Adaptation. In the natural world, visual sensors must cope with a wide dynamic range of irradiance, which can span on the order of 8 decades over the course of a day. Light variations within a scene are particularly challenging because they can make part of the visual field nonresponsive due to photoreceptor saturation. Animal retinæ partly solve this crucial problem by means of a local light adaptation mechanism integrated within each photoreceptor (3, 4, 25, 26). Similarly, we have equipped each prototype ommatidium with a neuromorphic adaptation circuit (Fig. S2D) that operates independent of its 629 neighbors. The neuromorphic circuit originally proposed by Delbrück and Mead (27) was modified here by cascading a first-order, low-pass filter (Fig. S2D). This modification prevents temporal aliasing and keeps the photodetector bandwidth of 300 Hz practically constant across the entire studied range of ambient lighting conditions. The circuit design was further optimized (SI Text, Photodetector Layer) to minimize the transient gain dispersion of each autoadaptive circuit. Fig. 4 shows the mean steady state and transient responses of 11 artificial ommatidia (photodetectors with optics) in one column to light step increments and decrements presented at four different steady light levels (Fig. S6). At each of these four levels (red circles in Fig. 4), the output response of the individual ommatidia to light steps yields an S-shaped operating curve in a semilog plot. Adaptation to a novel steady irradiance level essentially produces a horizontal shift of the curve without markedly changing its slope, which represents a dynamic sensitivity of about 1,300 mV per decade in the linear part. The steady operating curve (shown in red in Fig. 4) is also a logarithmic function of the adapting light, but with a slope (steady sensitivity) about 12-fold smaller. Thanks to the optimized design of the adaptive photodetector layout, the averaged dispersion of the sensitivity over the four operating curves is as small as 11 mV, that is, only about 2% of the total 600-mV dynamic range.

The four operating curves demonstrate not only the high sensitivity of the prototype ommatidia but their relative invariance in sensitivity to the ambient light. These $V(\log I)$ curves shifting with the operating points are reminiscent of those obtained in analogous

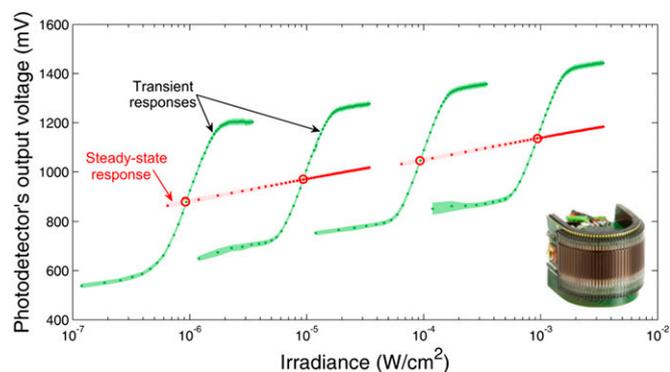


Fig. 4. CurvACE autoadaptation to ambient light at the single ommatidium level. Steady-state (red dots) and transient (green dots) responses of the adaptive analog VLSI photodetectors [design based on a circuit proposed by Delbrück and Mead (27)]. Each of the four dynamic operating curves (in green) shows the $V(\log I)$ response, averaged over 11 ommatidia (photodetectors with optics) of one column, to step increments and decrements of irradiance (Fig. S6) about four steady levels (red circles).

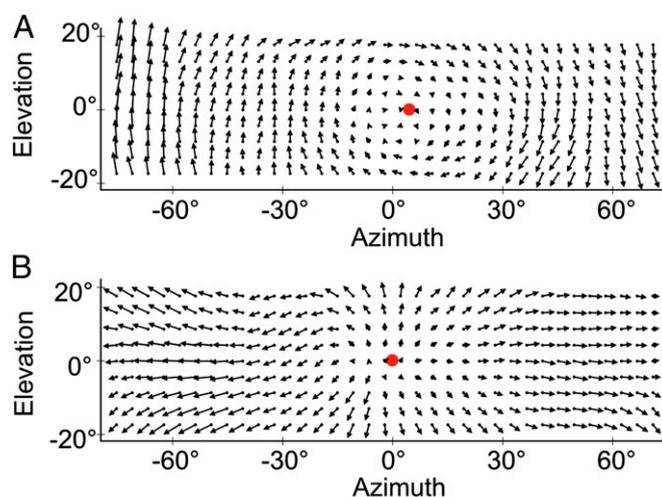


Fig. 5. Optic flow fields from the CurvACE prototype. Cylindrical equidistant projections of the optic flow field calculated with a modified version of the Lucas–Kanade method (29, 30) from the visual signals obtained by the CurvACE prototype subjected to roll motion (Fig. S8B) at 32° per second and at a distance of about 1 m to a wall displaying random black and white patterns (A) or to linear translation (Fig. S8C) at 3 cm/s toward the patterned wall at a distance of 1 cm (B). The red spot displays the center of rotation (A) or the focus of expansion (B).

experiments carried out on single vertebrate (25) and invertebrate (26) photoreceptors. This local adaptation is essential for efficient sampling of natural environments because it prevents saturation of the photoreceptors by bright spots in the visual scene while allowing them to adapt quickly to untoward illumination changes, such as transitions from a shaded area to a sunny place.

Characterization of Motion Extraction. In addition to an extensive FOV (Fig. 3) and local adaptation to illuminance (Fig. 4), the CurvACE prototype ommatidia yield a signal acquisition bandwidth of 300 Hz, which is threefold higher than that measured in the ommatidia of fast-flying insects (28). A high bandwidth contributes to the reduction of motion aliasing during fast locomotion. Furthermore, the implemented read-out protocol (Fig. S7) allows a maximum frame rate of 1.5 kfps, which permits frame averaging to improve the signal-to-noise ratio. We experimentally tested CurvACE motion detection capabilities by computing optic flow vectors from visual signals resulting from different types of motion in the presence of random black and white patterns on a wall (Fig. S8). In this first experiment, we used a modified version of the Lucas–Kanade method (29, 30) (SI Text, Optic Flow Characterization and Eqs. S1–S9), which is a particularly efficient image-based processing algorithm used to calculate optic flow vectors in two dimensions. The optic flow vectors measured during roll rotation (Fig. 5A) and linear translation toward a textured wall 0.3 s before collision (Fig. 5B) show coherent patterns of visual rotation and expansion, respectively. The center of rotation and focus of expansion can be clearly identified (red dots in Fig. 5), allowing for estimation of the axis of rotation and of the direction of translation, respectively. The sensor egomotion can be estimated from these flow fields, for instance, by implementing matched filters (31) analogous to the directionally selective, motion-sensitive neurons found in some insect visual systems (5). Furthermore, the embedded inertial sensors can be used for cancelling the rotational component of the measured optic flow, assessing only the translational component. Because this component is related to distance from objects, the optic flow data provided by a CurvACE prototype could assist mobile platforms to perform collision-free navigation (9).

We also characterized motion detection quantitatively at different ambient light levels with a bioinspired local visual processing

flying insects, would be especially interesting for egomotion estimation and better navigational support in three dimensions in a minimal package, providing an advantageous alternative to current cumbersome arrangements based on catadioptric or fish-eye lenses (9). A spherical CurvACE could be realized by fabricating and individually bending several ommatidial arrays with one ommatidium per column along the meridians of a sphere to measure optic flow omnidirectionally.

The CurvACE design is expected to foster further research and applications on fully flexible vision sensors (40, 41) that can adapt to rigid or unsteady surfaces of arbitrary shapes. Such devices could function as thin wearable sensors on smart clothing, as sensors for intelligent homes, or integrated in the artificial skin of soft robots. Toward these applications, future work could devise methods for cost-effective mass production of artificial ommatidia, which would also allow more complex dicing to achieve alternative bending patterns. Such production methods may in-

clude the realization of all processes of ommatidia alignment and assembly at the wafer level with the help of robotic platforms for automatized pick-and-place, bonding, and dicing.

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